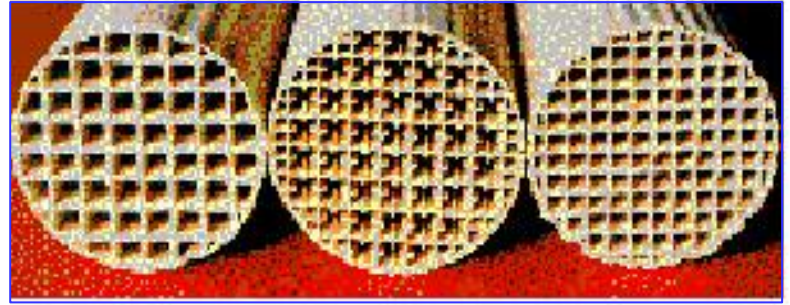
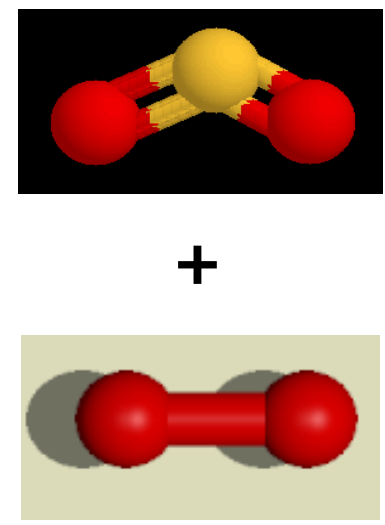


Transport-Kinetic Interactions for SO₂ Oxidation to SO₃ in Particulate and Monolith Catalysts

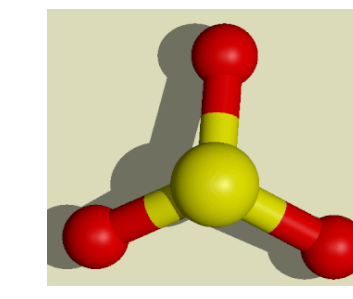
Monolith Catalysts



SO₂ Oxidation Catalysts



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SO₂ Oxidation Converter



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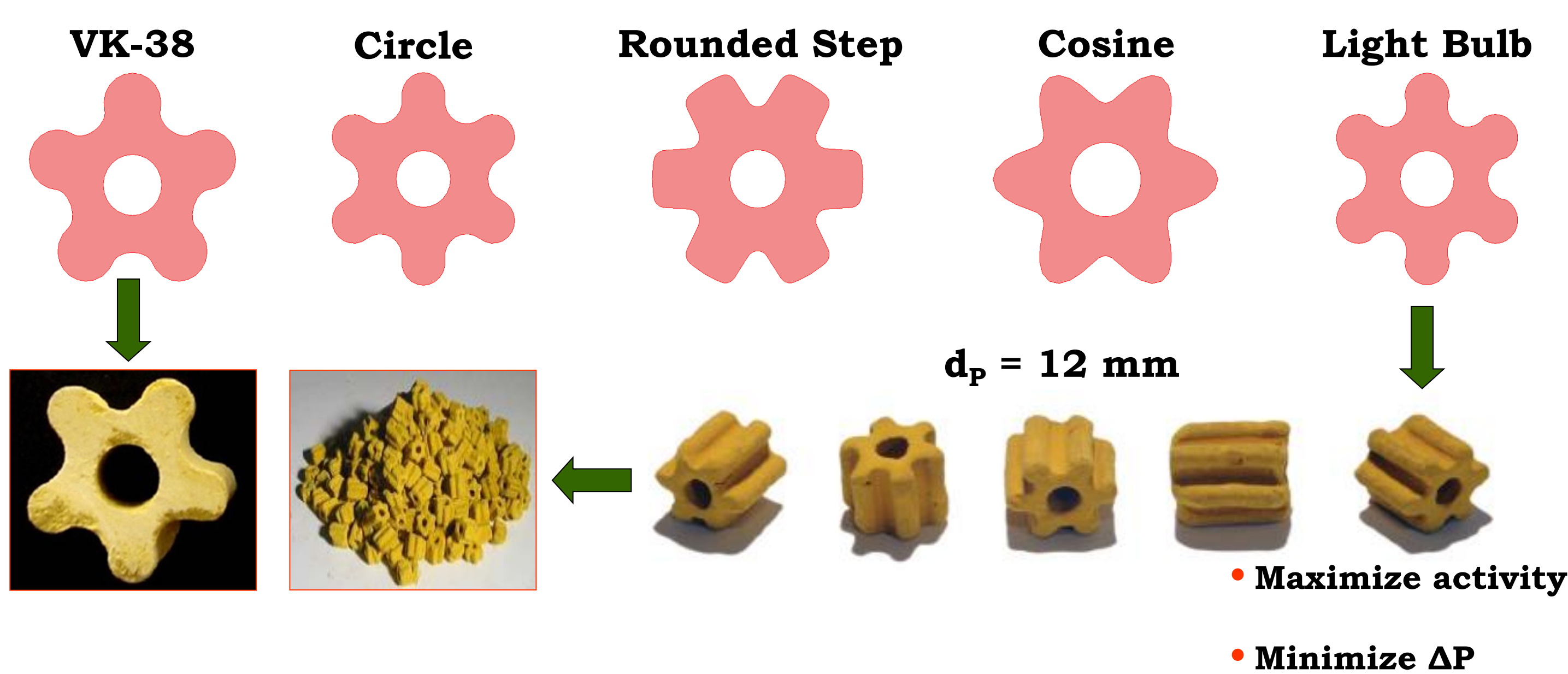
Introduction

Transport-kinetic interactions in commercial porous catalyst shapes used for SO₂ oxidation are analyzed using the Wilke, Wilke-Bosanquet, Maxwell-Stefan, and Dusty-Gas flux models. Particle effectiveness factors derived from the various flux models can differ for otherwise identical values for kinetic and transport parameters. Development of new catalysts having higher activity, lower pressure drop, and adequate crush strength to meet the anticipated reduction in SO₂ emissions from H₂SO₄ manufacturing plants will potentially benefit by using this more realistic approach for particle-scale shape modeling.

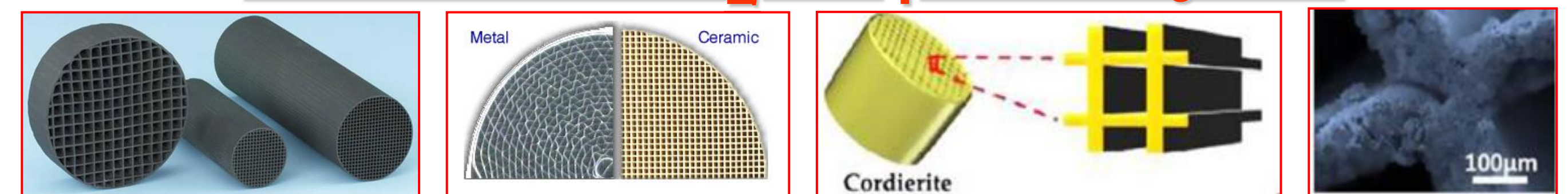
Objectives

- Review the current state-of-the art in modeling transport-kinetic interactions for catalyst particle shapes utilized in the SO₂ oxidation.
- Develop a rigorous modeling framework that accounts for diffusion and non-isothermal reaction in various realistic 3-D commercial catalyst shapes using different flux models.
- Employ this framework to compare the performance of these various catalyst shapes under typical multi-pass converter operation.

Catalyst Particle Shapes

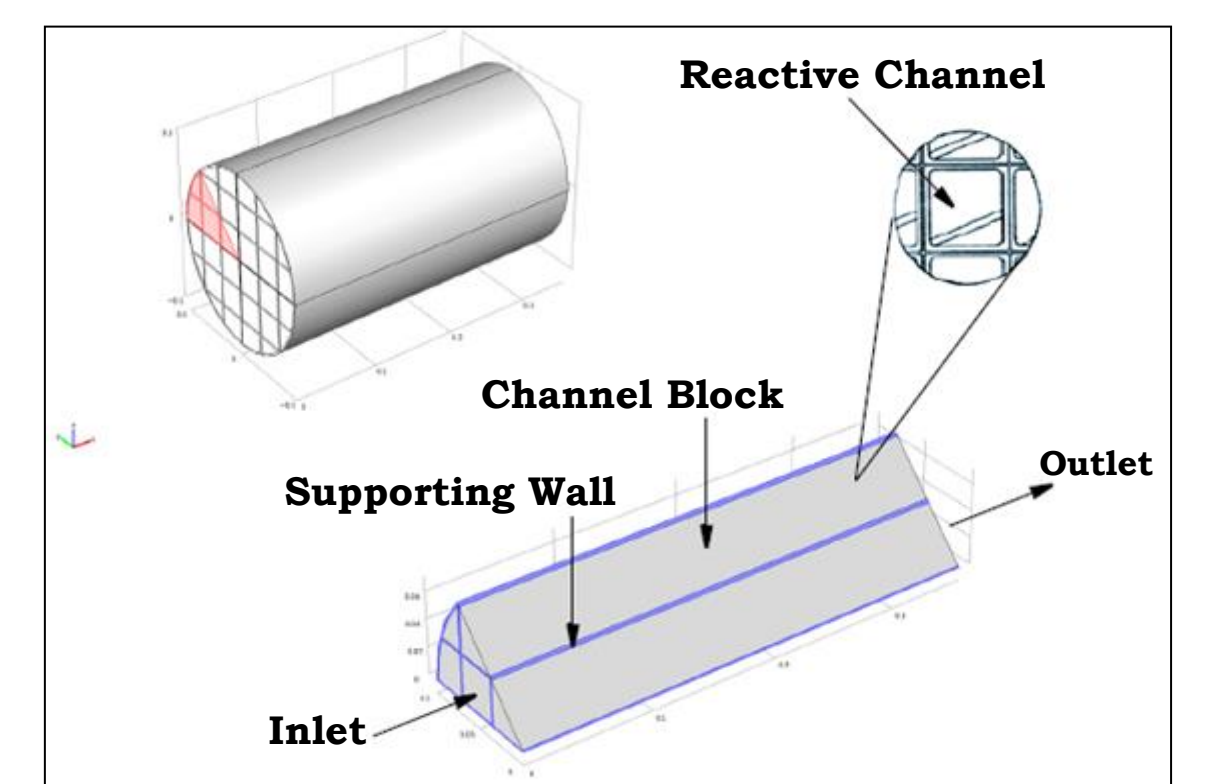


Monolith H₂SO₄ Catalysts



Modeling of SO₂ Oxidation in Honeycomb Structures

- In 1991, Beshpalov and coworkers* at Moscow Chemical Engineering Institute developed a numerical model for SO₂ oxidation in monolith catalysts.
- This is the only known open literature on SO₂ oxidation modeling for a monolith.
- An opportunity ALSO exists to **develop advanced models** for the purpose of design and analysis.



*Beshpalov, A.V. et al.(1991) Zhurnal Prikladnoi Khimii, 64(10) pp 2048 - 2053

Transport-Kinetics Particle Model

Species Mass Balance: $\nabla \cdot \mathbf{N}_i = \nu_i \mathbf{r} \rho_p$
where $i = \text{SO}_2, \text{O}_2, \text{SO}_3 \text{ \& } \text{N}_2$

Energy Balance: $\nabla \cdot \mathbf{q} = -(\Delta H_{rxn}) \mathbf{r} \rho_p$

SO₂ Oxidation Kinetics:
$$\mathbf{r} = \frac{k_1 p_{\text{O}_2} p_{\text{SO}_2} \left(1 - \frac{p_{\text{SO}_3}}{p_{\text{SO}_2} \sqrt{p_{\text{O}_2}} K_P}\right)}{22.414(1 + K_2 p_{\text{SO}_2} + K_3 p_{\text{SO}_3})^2}$$

T = 420 to 590°C

(Collina et al, 1971)

Diffusion Flux Models

Wilke Model

$$\mathbf{N}_i = (-D_{ei,m} \nabla C_i) \text{ where } D_{ei,m} = \frac{1}{\sum_{j=1, j \neq i}^n \left(\frac{x_j}{D_{ij}^e}\right)}$$

Wilke-Bosanquet Model

$$\mathbf{N}_i = (-D_{i,eff} \nabla C_i) \text{ where } \frac{1}{D_{i,eff}} = \frac{1}{D_{ei,m}} + \frac{1}{D_{ei,k}}$$

Maxwell-Stefan Model

$$\mathbf{N}_i = \frac{-\nabla C_i + \sum_{j=1, j \neq i}^n \frac{x_j \mathbf{N}_j}{D_{ij}^e}}{\sum_{j=1, j \neq i}^n \frac{x_j}{D_{ij}^e}}$$

Dusty-Gas Model

$$\mathbf{N}_i = \frac{\sum_{j=1, j \neq i}^n \frac{x_j \mathbf{N}_j}{D_{ij}^e} - \frac{C_i v^*}{D_{ei,k}} - \nabla C_i}{\sum_{j=1, j \neq i}^n \frac{x_j}{D_{ij}^e} + \frac{1}{D_{ei,k}}}$$

Effectiveness Factor
$$\eta = \frac{\int_0^{V_p} r(c, T) dV}{r(C_S, T_S) V_p}$$

Dimensionless Velocity
$$V^* = -\frac{\varepsilon d_{pore}^2}{32 \tau \mu} \nabla P$$

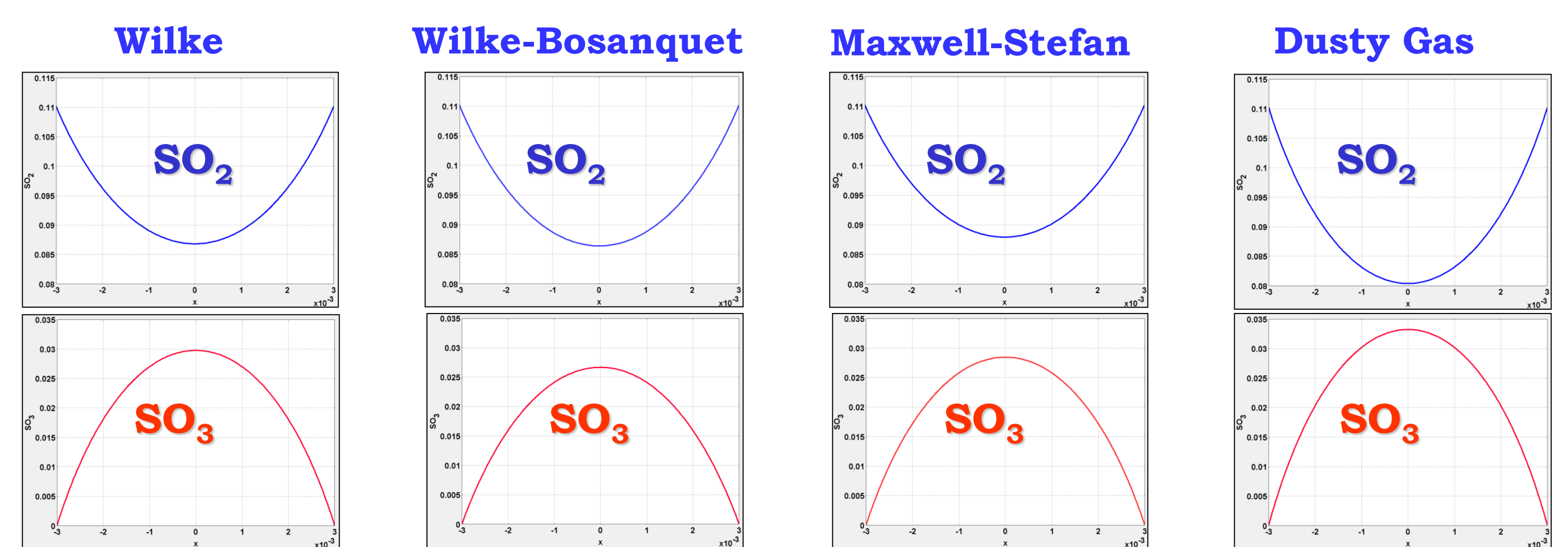
d_{pore} = 638 nm
ε = 0.44
τ = 2.7

*Reference: M. E. Davis, (1982) Chem. Eng. Sci., 37(3) pp 447-452

Results

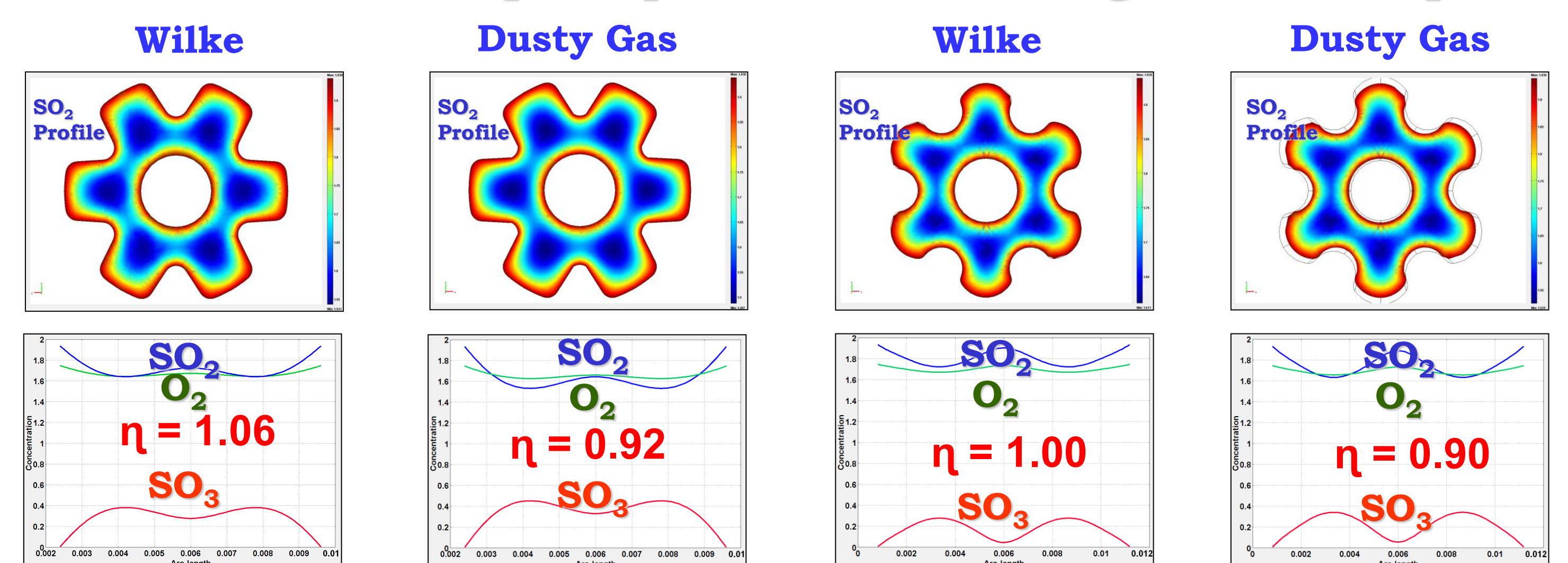
1-D Catalyst

T₀ = 420°C 11% SO₂ 9% O₂



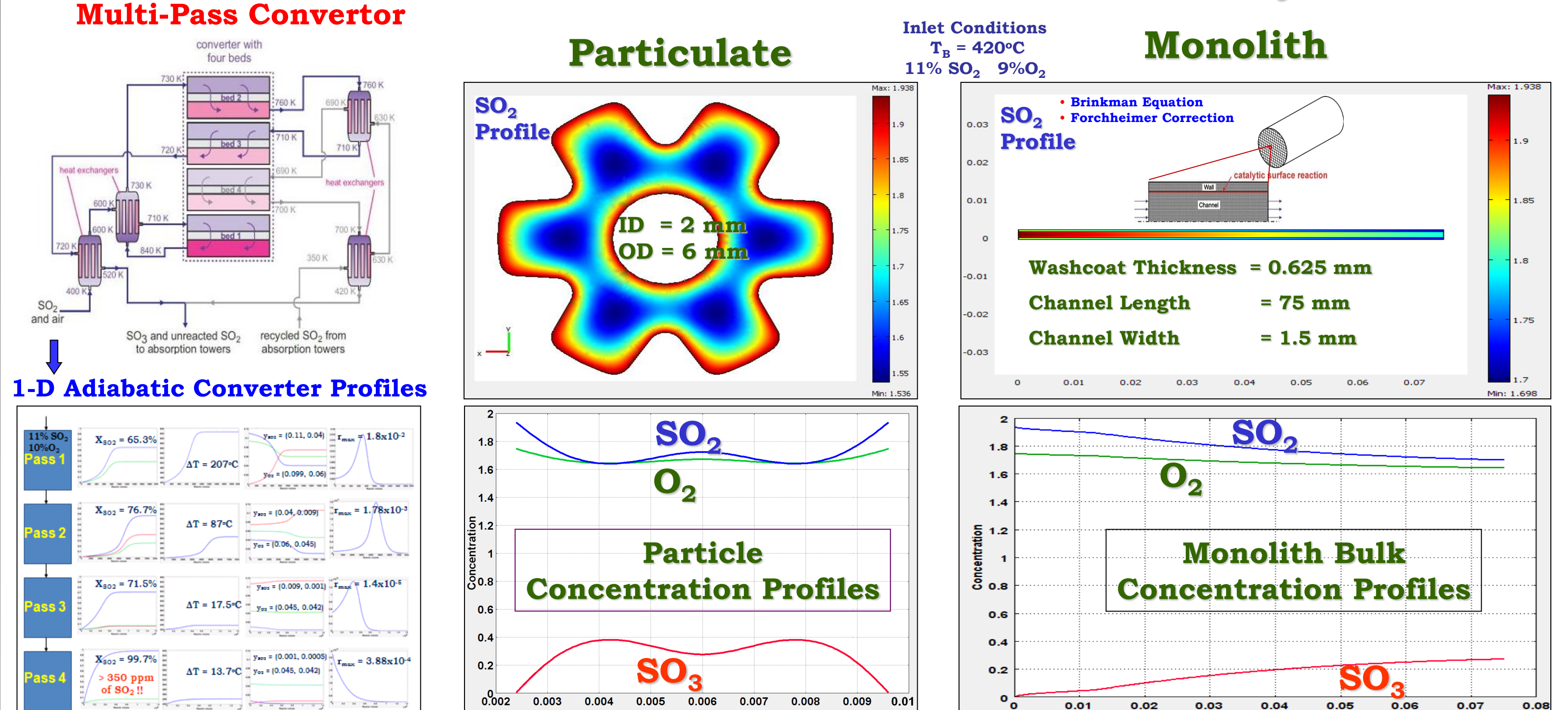
2-D Rounded Step Shape

2-D Light Bulb Shape



Commercial Multi-Pass Converter

Particulate vs Monolith Catalysts



CONCLUSIONS The Wilke model produces results that closely approximates those for the Dusty Gas Model for a uniform macroscopic pore structure for a given shape. However, the effectiveness factor varies with shape so it should be optimized in view of other factors, i.e., ΔP and crush strength. Detailed data on pore structure would be captured by the Dusty Gas Model. Monoliths provide another potential catalyst platform for SO₂ oxidation. Detailed models that account for transport-kinetic interactions can provide rationale approaches for comparing traditional particulate vs monolith reactor performance.