

Shape, Convection and Convergence

Roger W. Pryor, Ph.D., VP Research
Pryor Knowledge Systems, Inc.



Who is Pryor Knowledge Systems?

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- **A Technical Consultation firm in business since 1993**

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 - **Application of the unique properties of materials**

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- **Located in Southeast Michigan**

Overview:

I. Why solve this particular free convection problem?

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- II. How does a First Principles Analysis relate to this shape dependent model?

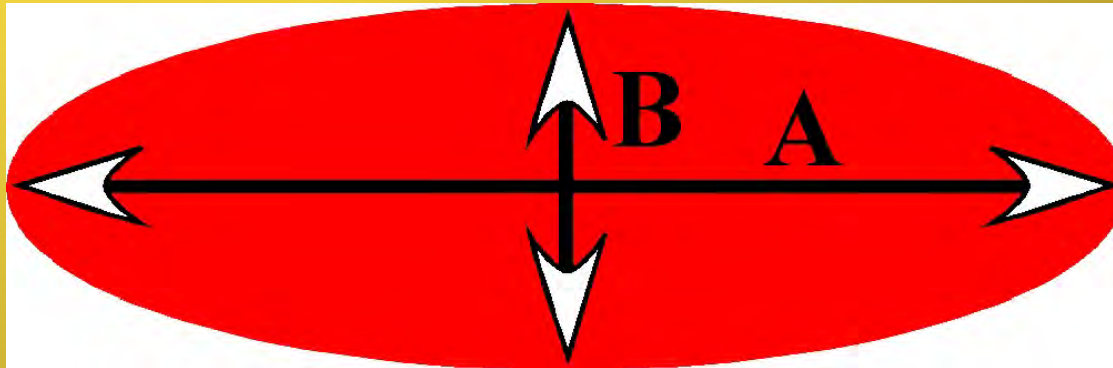
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- I. Why solve this particular free convection problem?
- II. How does a First Principles Analysis relate to this shape dependent model?
- III. How was the model built and solved?
- IV. What benefits are derived from applying this modeling technique?

Defining the Geometry of the Tank Top : What is the B/A Ratio?

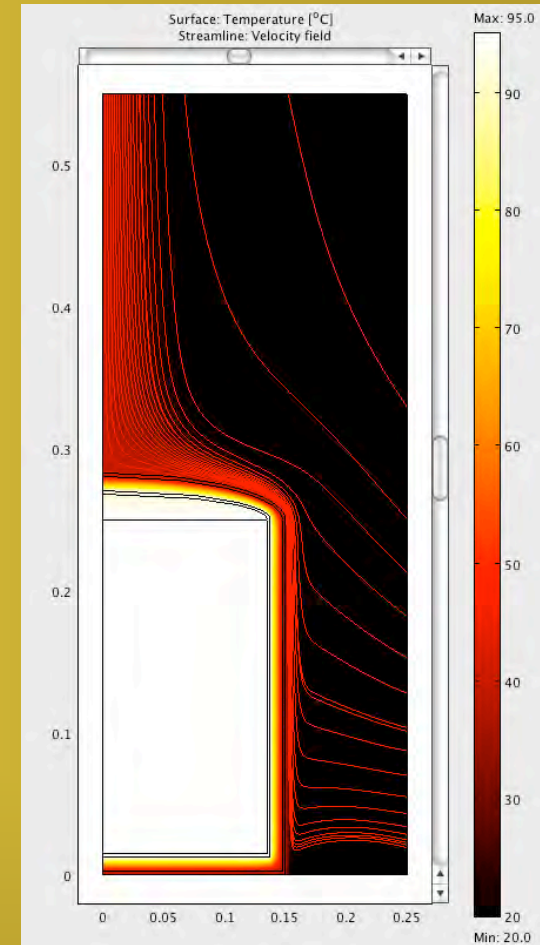


Geometric Specifications

Elliptical Tank Top : A-Semimajor, B-Semiminor

Introduction:

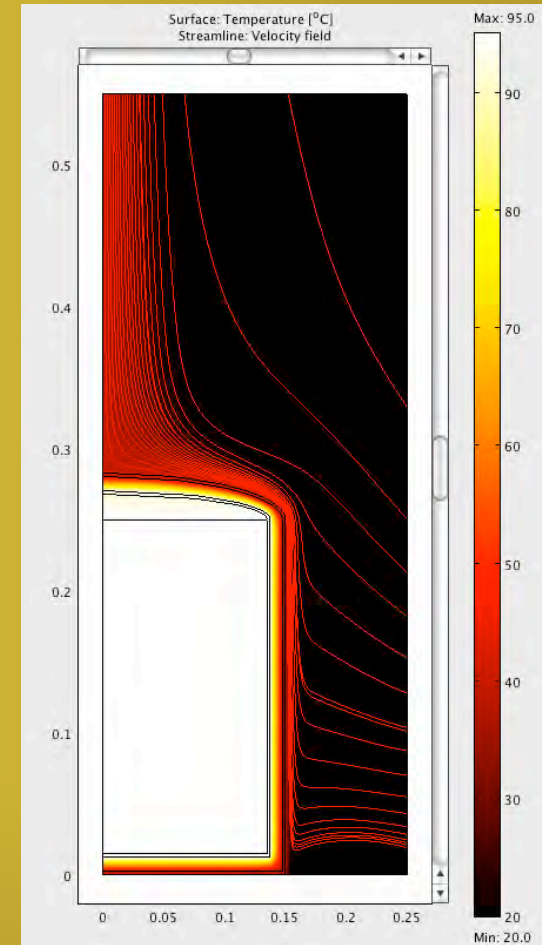
I. New Shape-Dependent Convection Model



**Navier-Stokes Streamline Patterns generated
by an Elliptically Shaped Tank Top**

Introduction:

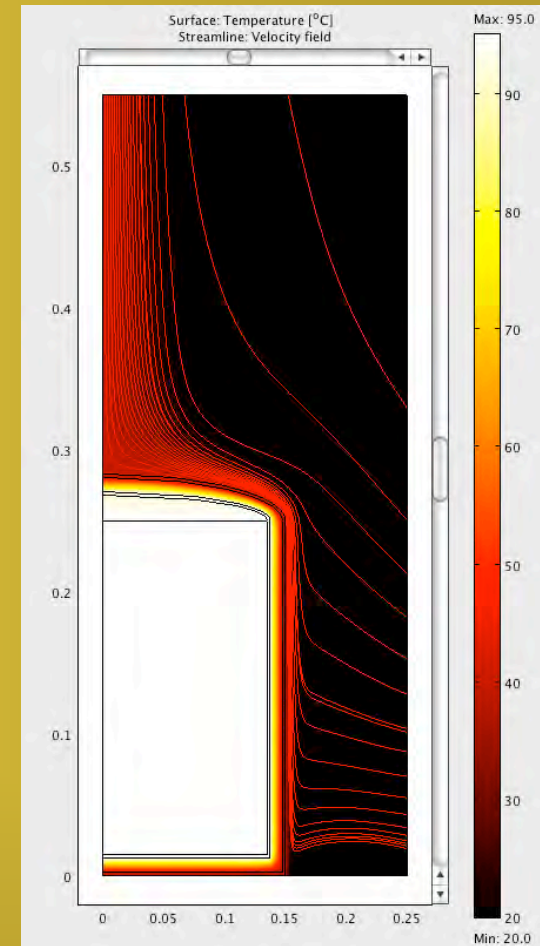
- I. New Shape-Dependent Convection Model
- II. 2D Axisymmetric Geometry



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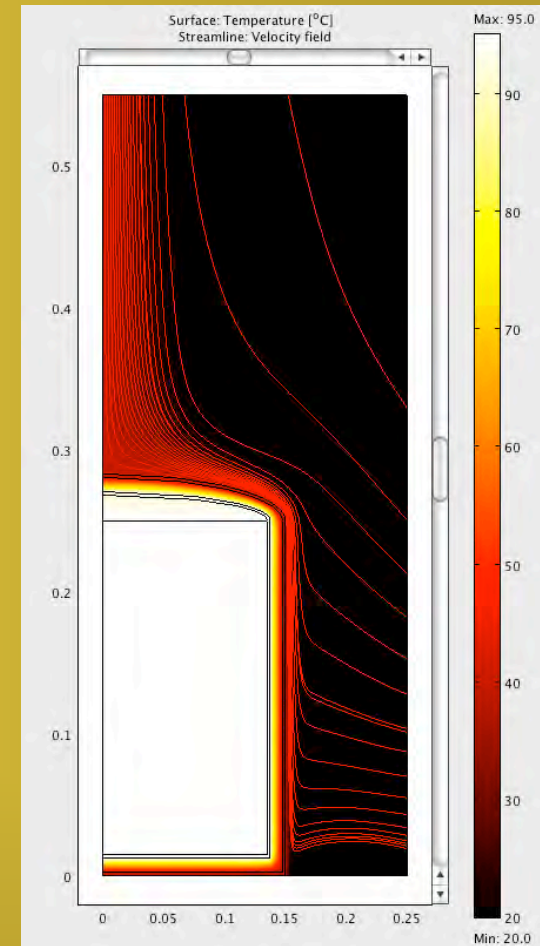
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Navier-Stokes Streamline Patterns generated by an Elliptically Shaped Tank Top

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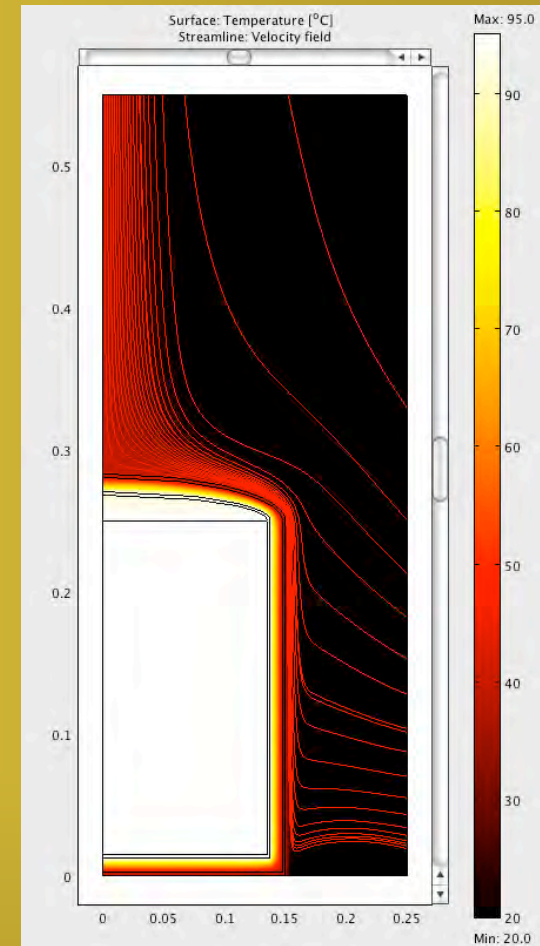
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Navier-Stokes Streamline Patterns generated by an Elliptically Shaped Tank Top

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- I. New Shape-Dependent Convection Model
- II. 2D Axisymmetric Geometry
- III. New Model Based on examples presented in: *thermos laminar hcoeff* and *thermos laminar flow* (Heat Transfer Module Model Library (COMSOL 3.4))
- IV. Shape Ratio (B/A) Varied by changes in the Elliptical Tank Top
- V. Shape-Dependent Model Convergence determined by both Tank Top Shape (B/A Ratio) and Modified Solver Parameters



Navier-Stokes Streamline Patterns generated by an Elliptically Shaped Tank Top

First Principles Applied to Fluid Flow

- I. Calculation of fluid flow behavior is a complex and mathematically difficult area to model.**

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- II. First Principles Analysis determines predominant contributing factors.**
- III. In this problem, the surface geometry (shape) of the top of the tank (B/A ratio) is the primary governing factor.**

The Physics:

I. Free Convection

The Physics:

I. Free Convection

II. Driving Forces:

a) temperature differential

The Physics:

I. Free Convection

II. Driving Forces:

- a) temperature differential
- b) differential density

The Physics:

I. Free Convection

II. Driving Forces:

- a) temperature differential
- b) differential density
- c) geometry of the flow path

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I. Free Convection

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- c) geometry of the flow path
- d) gravitational force

The Physics:

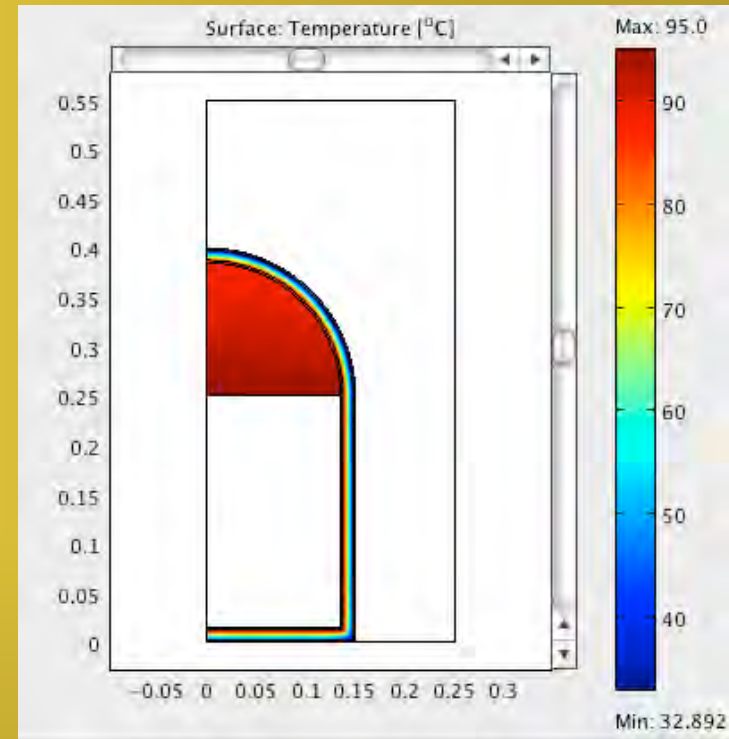
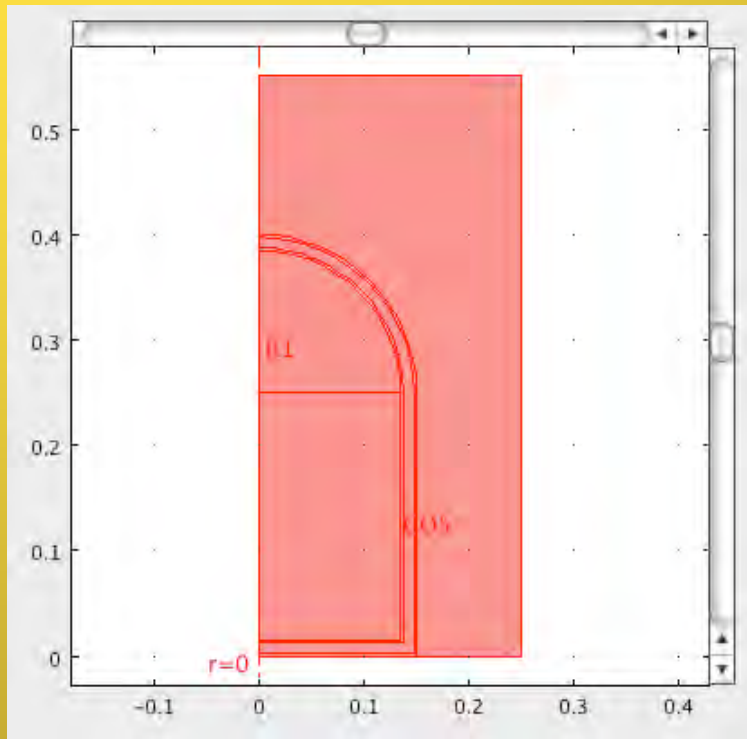
I. Free Convection

II. Driving Forces:

- a) temperature differential**
- b) differential density**
- c) geometry of the flow path**
- d) gravitational force**

III. Tank (water) Temperature

COMSOL Heat Transfer Model 1:

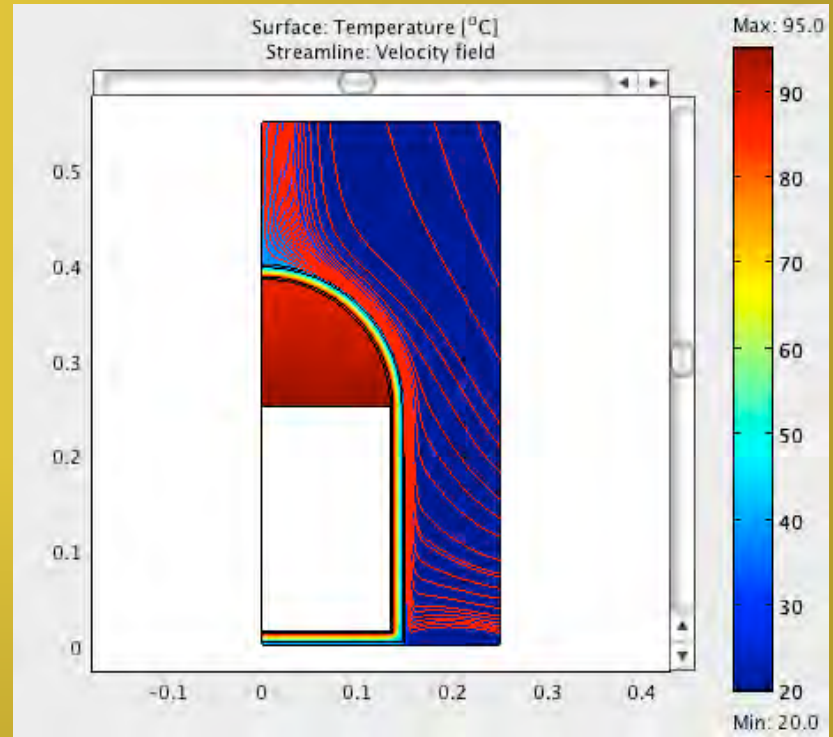
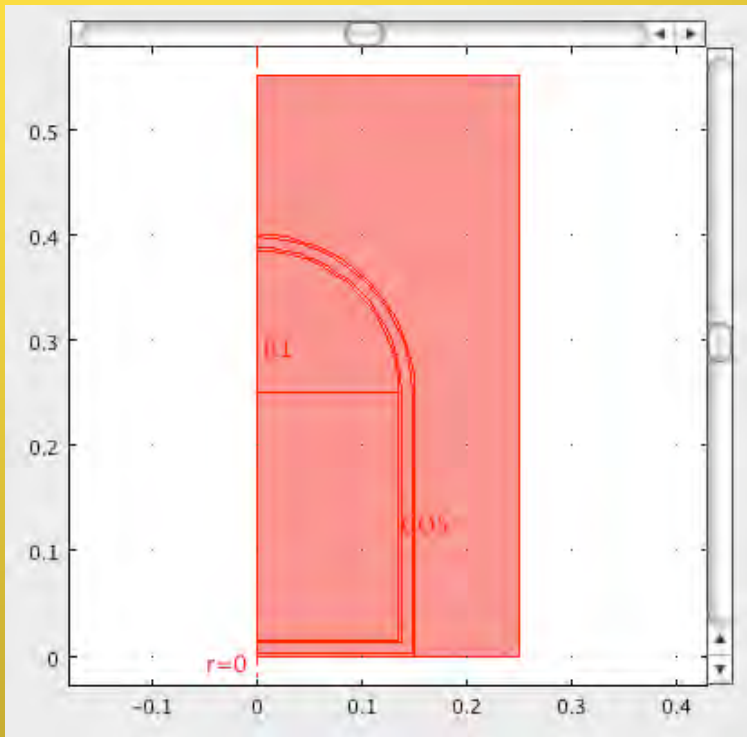


Tank Top B/A Ratio = 1.0

2D Axisymmetric Heat Transfer Initialization Model

Model 1 - Accurate Heat Transfer Results

COMSOL Navier-Stokes Model 2:



Tank Top B/A Ratio = 1.0

2D Axisymmetric Free Convection Model

Model 2 - Accurate Convection Results

Model Constants:

Name	Value	Description
k_insul	0.01[W/(m*K)]	k (Insulation)
p_atm	1[atm]	Air pressure
Length	0.4[m]	Height of tank*
T_water	95[degC]	Water Temperature
T_amb	20[degC]	Ambient Temperature
rho_insul	60[kg/m^3]	Density (Insulation)
Cp_insul	200[J/(kg*K)]	Heat Capacity (Insulation)
Length2	0.15[m]	Width of Tank

*This is the projected height and varies for different tank configurations: $Length = B(\text{Semi-axis length}) + \text{Height (Tank Rectangle)}$

Model Scalar Expressions:

Name	Expression
F_buoyancy*	9.81[m/s²]*(rho_air_ref-rho_chns)
rho_air_ref**	mat2_rho(p_atm[1/Pa],T_amb[1/K])[kg/m³]

*Buoyancy Force

** Density of Air @ STP

Setting up the Geometry for Models 1&2:

Tank Top Configuration (TTC) #	A[m]	B[m]	B/A	Convergence
1	0.15	0.15	1	Yes
2	0.15	0.20	1.33	Yes
3	0.15	0.05	0.33	Yes
4	0.15	0.03	0.20	HT: Yes N-S: No
5	0.15	0.04	0.267	Yes
6	0.15	0.033	0.22	Yes

Elliptical Tank Top Geometric Specifications

The Models 1&2 Geometry:

Models 1&2

$B/A = 1$

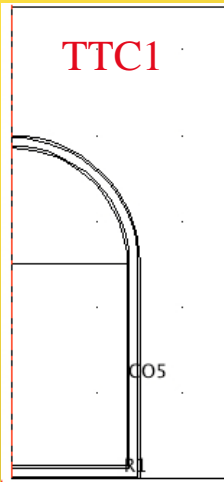
Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

The Models 1&2 Geometry:

Models 1&2

$$B/A = 1$$

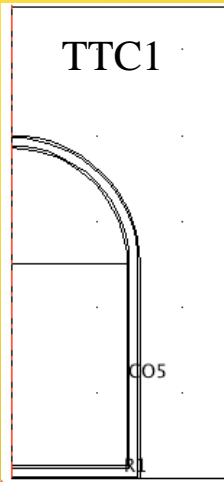
Length =

$$0.4[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = Yes



Models 1&2

$$B/A = 1.33$$

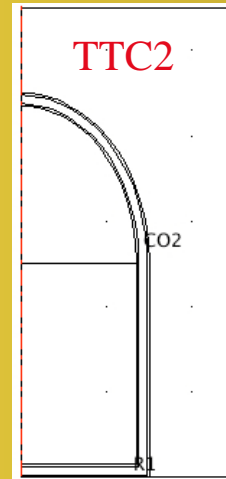
Length =

$$0.45[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = Yes



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$$B/A = 1$$

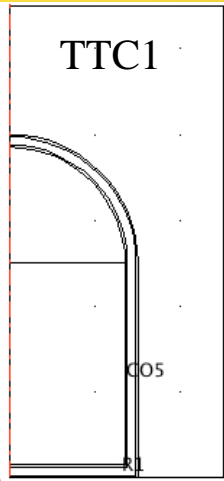
Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



Models 1&2

$$B/A = 1.33$$

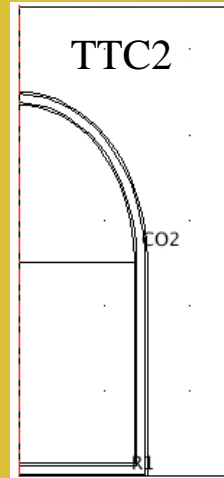
Length =

0.45[m]

Length2 =

0.15[m]

C = Yes



Models 1&2

$$B/A = 0.33$$

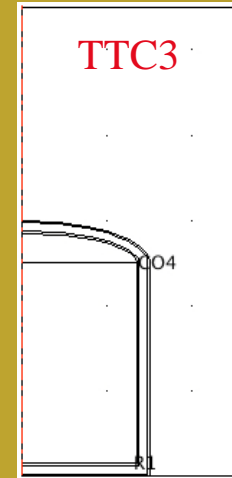
Length =

0.30[m]

Length2 =

0.15[m]

C = Yes



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

The Models 1&2 Geometry:

Models 1&2

$$B/A = 1$$

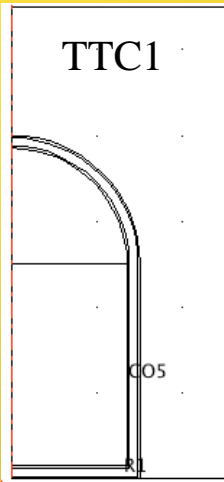
Length =

$$0.4[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = Yes



Models 1&2

$$B/A = 1.33$$

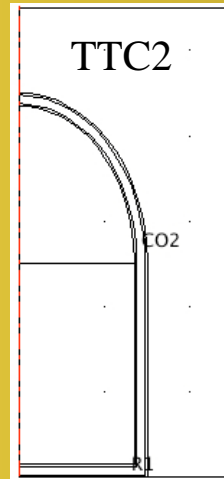
Length =

$$0.45[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = Yes



Models 1&2

$$B/A = 0.33$$

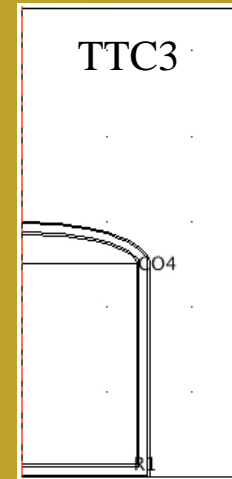
Length =

$$0.30[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = Yes



Models 1&2

$$B/A = 0.20$$

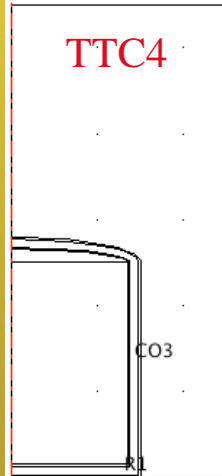
Length =

$$0.28[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = No



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

The Models 1&2 Geometry:

Models 1&2

$$B/A = 1$$

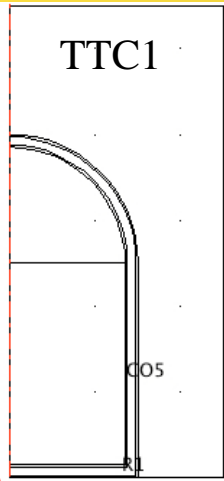
Length =

$$0.4[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = Yes



Models 1&2

$$B/A = 1.33$$

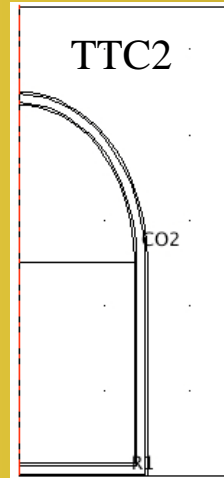
Length =

$$0.45[\text{m}]$$

Length2 =

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C = Yes



Models 1&2

$$B/A = 0.33$$

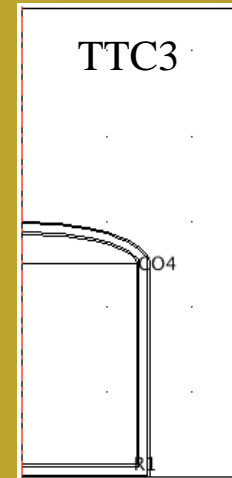
Length =

$$0.30[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = Yes



Models 1&2

$$B/A = 0.20$$

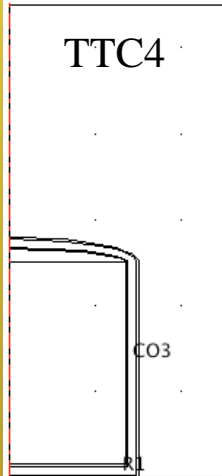
Length =

$$0.28[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = No



Models 1&2

$$B/A = 0.267$$

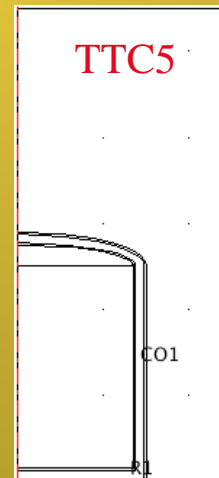
Length =

$$0.29[\text{m}]$$

Length2 =

$$0.15[\text{m}]$$

C = Yes



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

The Models 1&2 Geometry:

Models 1&2

$$B/A = 1$$

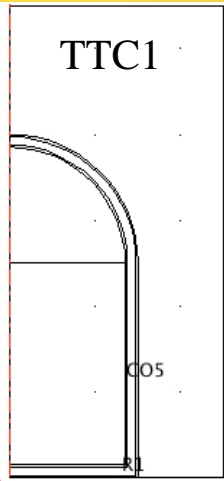
Length =

$$0.4[m]$$

Length2 =

$$0.15[m]$$

C = Yes



Models 1&2

$$B/A = 1.33$$

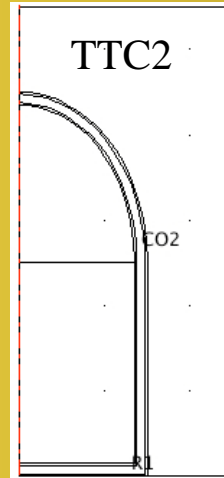
Length =

$$0.45[m]$$

Length2 =

$$0.15[m]$$

C = Yes



Models 1&2

$$B/A = 0.33$$

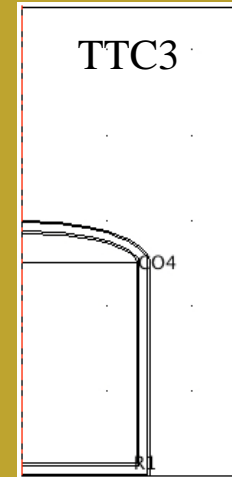
Length =

$$0.30[m]$$

Length2 =

$$0.15[m]$$

C = Yes



Models 1&2

$$B/A = 0.20$$

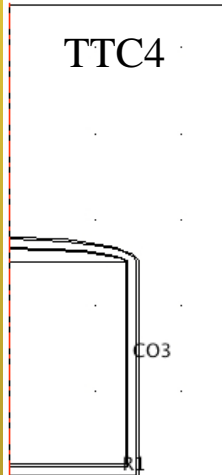
Length =

$$0.28[m]$$

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C = No



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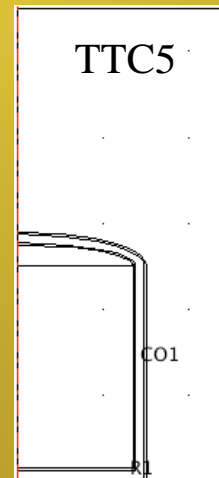
Length =

$$0.29[m]$$

Length2 =

$$0.15[m]$$

C = Yes



Models 1&2

$$B/A = 0.22$$

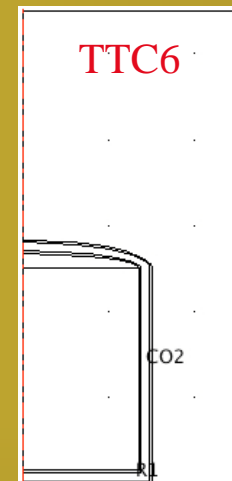
Length =

$$0.283[m]$$

Length2 =

$$0.15[m]$$

C = Yes



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

Setting up the Physics Subdomain

Model 1(HT):

Subdomain #	Source	Material
1	BML**	structural steel
2	Constants	k_insul rho_insul Cp_insul
3	BML	structural steel
5	BML	Air*

** (BML) Basic Materials Library

*replace p with p_atm

Setting up the Physics Boundary Settings

Model 1(HT):

Boundary	Condition	Setting
8, 14, 20	Temperature	T_water in T₀ edit window
23	Heat Flux	Load h: Nat. Vertical wall, L=height Change L_htgh to Length Enter T_amb in T_{inf} edit window
29	Heat Flux	Load h: Nat Horiz. plane, Upside, L=width Change L_htgh to Length2 Enter T_amb in T_{inf} edit window

Meshing and Solving Model 1(HT):

Use the default Mesh and Solver Parameters

Click Solve

Model 1(HT):Solutions

Model 1

$B/A = 1$

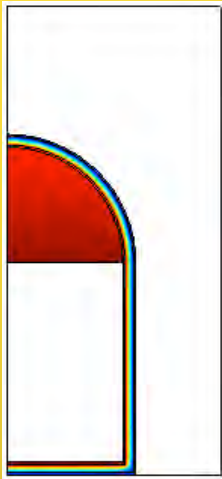
Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



Model 1(HT):Solutions

Model 1

B/A = 1

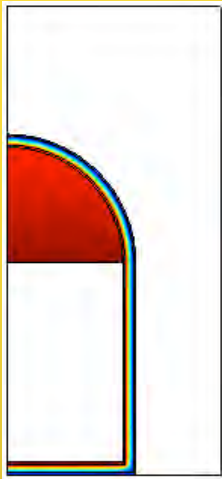
Length =

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Length2 =

0.15[m]

C = Yes



Model 1

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Length =

0.45[m]

Length2 =

0.15[m]

C = Yes



Model 1(HT):Solutions

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B/A = 1

Length =

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Length2 =

0.15[m]

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Model 1

B/A = 1.33

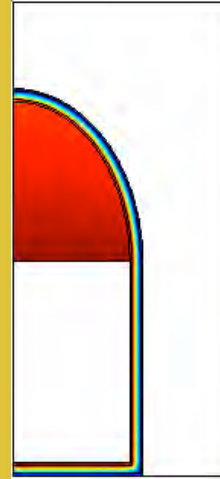
Length =

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Model 1

B/A = 0.33

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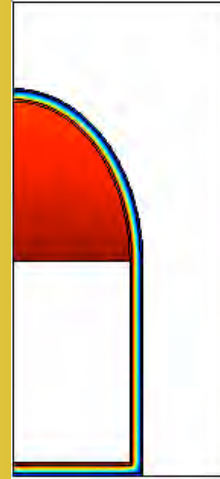
Length =

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Length2 =

0.15[m]

C = Yes



Model 1

B/A = 0.33

Length =

0.30[m]

Length2 =

0.15[m]

C = Yes



Model 1

B/A = 0.20

Length =

0.28[m]

Length2 =

0.15[m]

C = Yes



Model 1(HT):Solutions

Model 1

B/A = 1

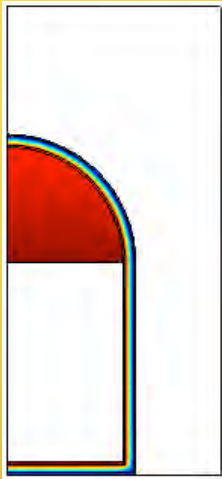
Length =

0.4[m]

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0.15[m]

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Model 1

B/A = 1.33

Length =

0.45[m]

Length2 =

0.15[m]

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Model 1

B/A = 0.33

Length =

0.30[m]

Length2 =

0.15[m]

C = Yes



Model 1

B/A = 0.20

Length =

0.28[m]

Length2 =

0.15[m]

C = Yes



Model 1

B/A = 0.267

Length =

0.29[m]

Length2 =

0.15[m]

C = Yes



Model 1(HT):Solutions

Model 1

B/A = 1

Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



Model 1

B/A = 1.33

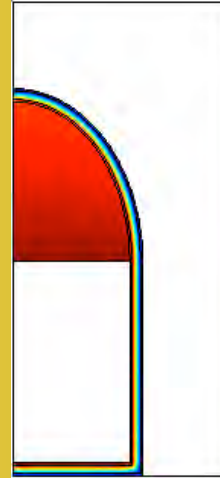
Length =

0.45[m]

Length2 =

0.15[m]

C = Yes



Model 1

B/A = 0.33

Length =

0.30[m]

Length2 =

0.15[m]

C = Yes



Model 1

B/A = 0.20

Length =

0.28[m]

Length2 =

0.15[m]

C = Yes



Model 1

B/A = 0.267

Length =

0.29[m]

Length2 =

0.15[m]

C = Yes



Model 1

B/A = 0.22

Length =

0.283[m]

Length2 =

0.15[m]

C = Yes



Model 2: Building a Navier-Stokes Multiphysics Model(s)

**Do the following steps for each of the
HT configurations (1-6):**

Multiphysics>

Model Navigator>

Heat Transfer Module>

Weakly Compressible Navier-Stokes>

Steady-state analysis>

Click Add>

Click OK.

Setting up the Physics Subdomain in each Model 2 (N-S) configuration:

Subdomain #	Source	Material
1-5	Inactive	
6	BML	Air* $F_z = F_{\text{buoyancy}}$

>Click the Density tab>

** (BML) Basic Materials Library

*replace $\rho(p[...]$ with $\rho((p+p_{\text{atm}})[...]$

Model 2: Physics Settings HT Subdomain Settings

Do the following steps for each of the N-S configurations (1-6):

Multiphysics>General Heat Transfer>Physics>Subdomain settings

Select: Subdomain 6>Select the Active in this domain check box.

Select: Air from the Library material list.

Model 2: Physics Settings HT Subdomain Settings

Do the following steps for each of the N-S configurations (1-6):

Multiphysics>General Heat Transfer>Physics>Subdomain settings

Select: Subdomain 6>Select the Active in this domain check box.

Select: Air from the Library material list.

Click the Convection tab.

Select: Enable convective heat transfer check box.

Replace: $\rho(p[...$ with $\rho((p+p_{atm})[...$

In the Density edit window. Click Apply

Enter: u and v in the Velocity field edit windows.

Model 2: Physics Settings HT Subdomain Settings

Do the following steps for each of the N-S configurations (1-6):

Multiphysics>General Heat Transfer>Physics>Subdomain settings

Select: Subdomain 6>Select the Active in this domain check box.

Select: Air from the Library material list.

Click the Convection tab.

Select: Enable convective heat transfer check box.

Replace: $\rho(p[...$ with $\rho((p+p_{atm})[...$

In the Density edit window. Click Apply

Enter: u and v in the Velocity field edit windows.

Click the Artificial Diffusion button.

Select: Streamline diffusion check box.

Select: Galerkin least-squares (GLS) from the list.

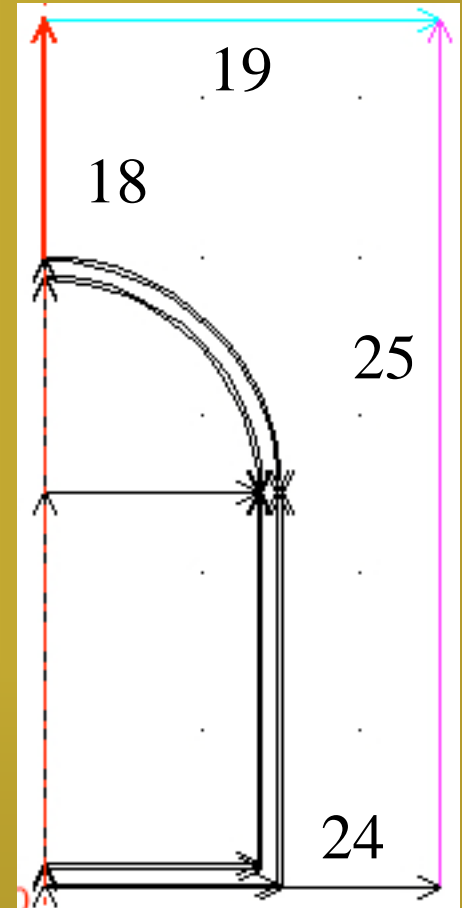
Model 2: Physics Settings

HT Boundary Conditions

Do the following steps for each of the N-S configurations (1-6):

Select: Multiphysics>
General Heat Transfer>
Physics>Boundary Settings.

Boundary	Condition
18	Axial Symmetry
19	Convective Flux
24	Thermal Insulation
25	Temperature Enter T_{amb} in the T_0 edit window



Model 2: Physics Settings

N-S Boundary Conditions

Do the following steps for each of the N-S configurations (1-6):

Select: Multiphysics> Weakly Compressible Navier-Stokes>Boundary Settings.

Boundary	Boundary Type	Boundary Condition
18	Symmetry boundary	Axial Symmetry
19	Outlet	Normal stress f_0 to 0
25	Open boundary	Normal stress f_0 to 0
23, 24, 29	Wall	No slip

Model 2 Mesh Generation:

Select: Mesh>Free Mesh Parameters

Select: Subdomain tab

In the **Subdomain selection** window, **Select:**

Subdomain 6 >

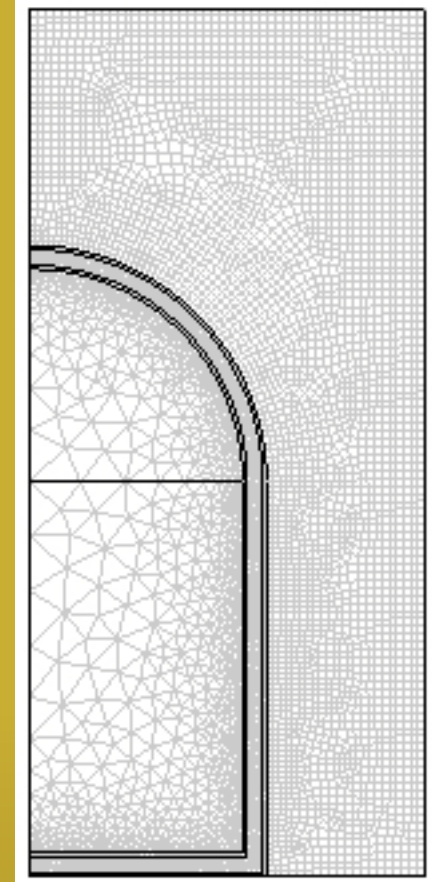
Enter **0.005** in the

Subdomain mesh parameters edit window>

Select: Quad>

Click the Remesh button>

Click OK



**Quad Mesh generated for an
Elliptically Shaped Tank Top
B/A = 1.0**

Solver Parameters:

Click the Stationary tab

Select: Damped Newton, Highly nonlinear problem,

Manual tuning of damping parameters Check boxes

Solver Parameters:

Click the Stationary tab

**Select: Damped Newton, Highly nonlinear problem,
Manual tuning of damping parameters Check boxes**

Enter:

Relative tolerance	1.0E-2
Maximum iterations	50
Initial damping factor	1.0E-4
Minimum damping factor	1.0E-12

Solver Parameters:

Click the Stationary tab

**Select: Damped Newton, Highly nonlinear problem,
Manual tuning of damping parameters Check boxes**

Enter:

Relative tolerance	1.0E-2
Maximum iterations	50
Initial damping factor	1.0E-4
Minimum damping factor	1.0E-12

Click Advanced tab

Type of scaling **none**

Click OK

Select: Solve

Navier-Stokes Free Convection Solutions:

Models 2

$B/A = 1$

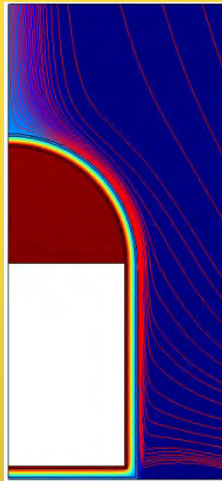
Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

Navier-Stokes Free Convection Solutions:

Models 2

$B/A = 1$

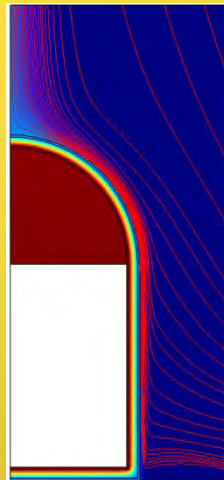
Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



Models 2

$B/A = 1.33$

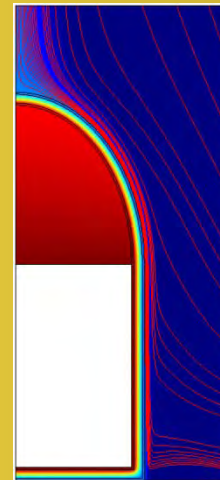
Length =

0.45[m]

Length2 =

0.15[m]

C = Yes



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

Navier-Stokes Free Convection Solutions:

Models 2

$B/A = 1$

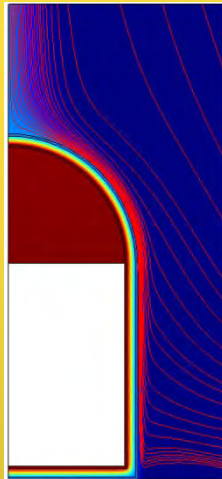
Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



Models 2

$B/A = 1.33$

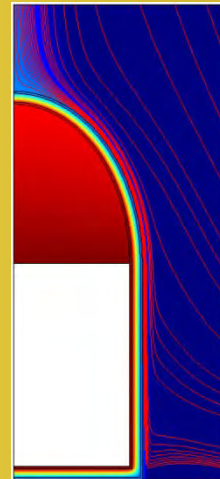
Length =

0.45[m]

Length2 =

0.15[m]

C = Yes



Model 2

$B/A = 0.33$

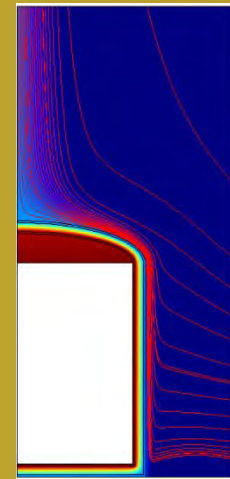
Length =

0.30[m]

Length2 =

0.15[m]

C = Yes



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

Navier-Stokes Free Convection Solutions:

Models 2

B/A = 1

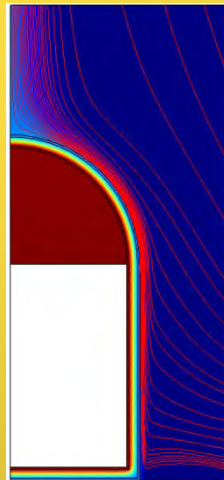
Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



Models 2

B/A = 1.33

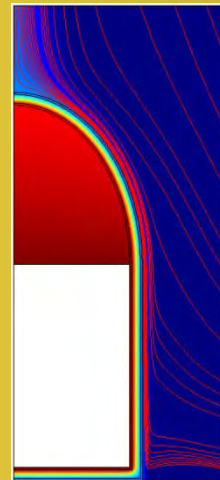
Length =

0.45[m]

Length2 =

0.15[m]

C = Yes



Model 2

B/A = 0.33

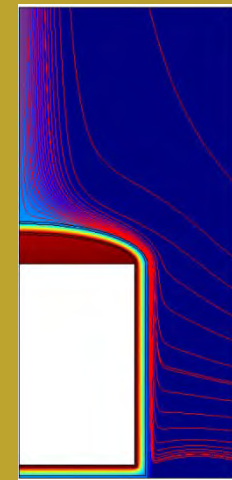
Length =

0.30[m]

Length2 =

0.15[m]

C = Yes



Model 2

B/A = 0.20

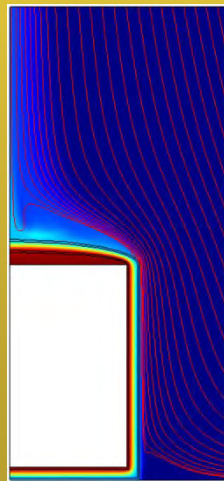
Length =

0.28[m]

Length2 =

0.15[m]

C = No



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

Navier-Stokes Free Convection Solutions:

Models 2

$B/A = 1$

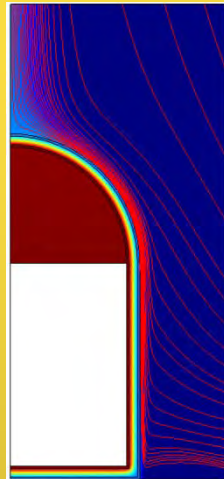
Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



Models 2

$B/A = 1.33$

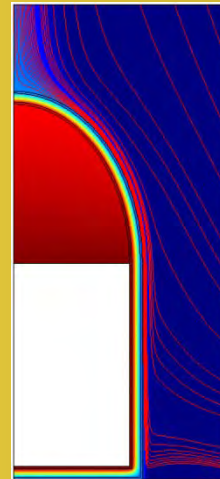
Length =

0.45[m]

Length2 =

0.15[m]

C = Yes



Model 2

$B/A = 0.33$

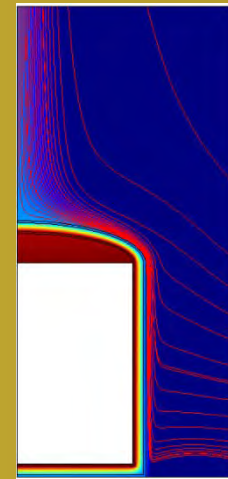
Length =

0.30[m]

Length2 =

0.15[m]

C = Yes



Model 2

$B/A = 0.20$

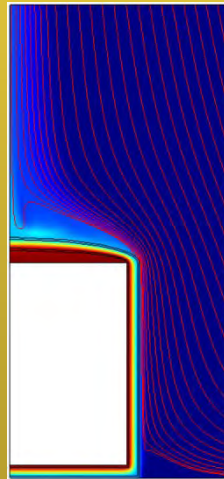
Length =

0.28[m]

Length2 =

0.15[m]

C = No



Model 2

$B/A = 0.267$

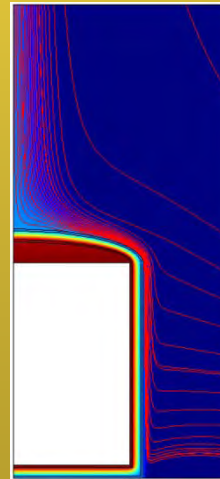
Length =

0.29[m]

Length2 =

0.15[m]

C = Yes



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

Navier-Stokes Free Convection Solutions:

Models 2

$B/A = 1$

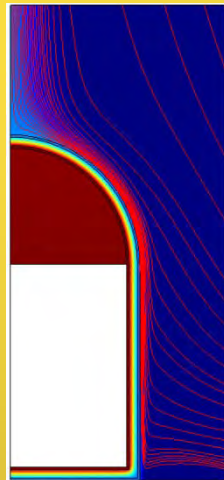
Length =

0.4[m]

Length2 =

0.15[m]

C = Yes



Models 2

$B/A = 1.33$

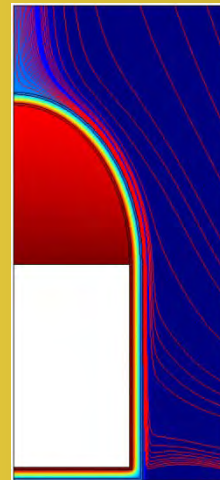
Length =

0.45[m]

Length2 =

0.15[m]

C = Yes



Model 2

$B/A = 0.33$

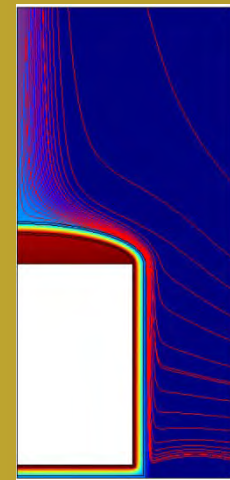
Length =

0.30[m]

Length2 =

0.15[m]

C = Yes



Model 2

$B/A = 0.20$

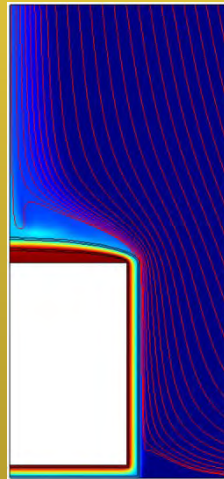
Length =

0.28[m]

Length2 =

0.15[m]

C = No



Model 2

$B/A = 0.267$

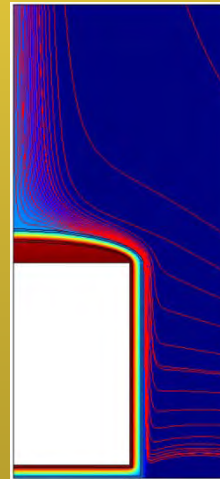
Length =

0.29[m]

Length2 =

0.15[m]

C = Yes



Model 2

$B/A = 0.22$

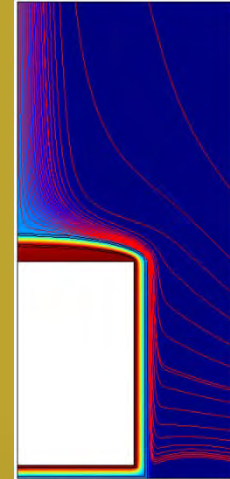
Length =

0.283[m]

Length2 =

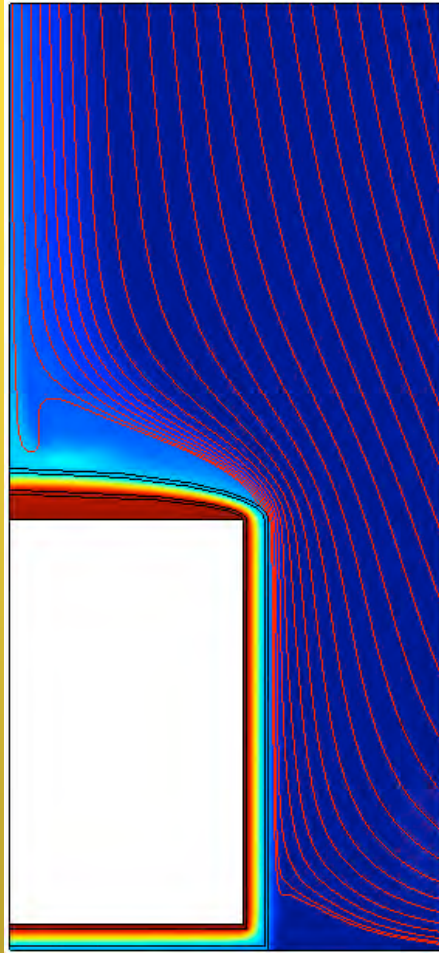
0.15[m]

C = Yes



2D Axisymmetric Elliptical Tank Top Model Cross-Sections

Conclusions



Non-Convergent

Model 2

$B/A = 0.22$

Length =

0.283[m]

Length2 =

0.15[m]



Model 2

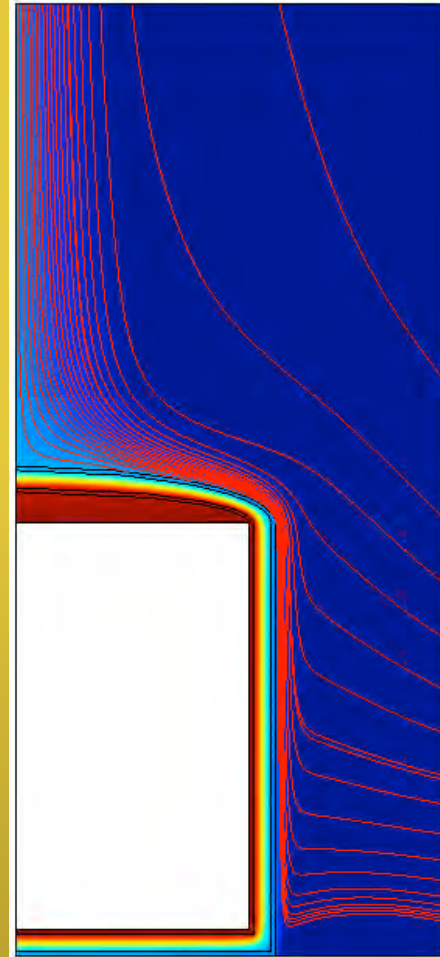
$B/A = 0.20$

Length =

0.28[m]

Length2 =

0.15[m]



Convergent

Successful implementation of a model is dependent on small parametric differences.

2D Axisymmetric Elliptical Tank Top Model Cross-Sections

**Thank
you!**